

①

# Mécanisme tournant

$$1] \vec{\omega} = -\frac{L}{R} \dot{\varphi} \vec{e}_3; \quad \vec{\Omega}_{2/1} = \vec{\omega} + \dot{\varphi} \vec{e}_2 = -\frac{L}{R} \dot{\varphi} \vec{x}_2 + \dot{\varphi} \vec{e}_2$$

$$2] \vec{R}_A(2/1) = \vec{0} \quad (\text{centre d'inertie en } A)$$

$$\vec{f}(A, 2/1) = G_2 \ddot{\varphi} \vec{e}_2$$

$$3] \vec{v}(C \in 3/1) = L \dot{\varphi} \vec{y}_2$$

$$\vec{p}_A(3/1) = m_3 L (\ddot{\varphi} \vec{y}_2 - \dot{\varphi}^2 \vec{x}_2)$$

$$\vec{T}(G_1, 3/1) = \begin{bmatrix} A_3 & & \\ & B_3 & \\ & & B_3 \end{bmatrix} \begin{bmatrix} -\frac{L}{R} \dot{\varphi} \\ 0 \\ \dot{\varphi} \end{bmatrix} = -\frac{L}{R} A_3 \dot{\varphi} \vec{x}_2 + B_3 \dot{\varphi} \vec{e}_2$$

$$\vec{f}(G_1, 3/1) = -\frac{L}{R} A_3 \ddot{\varphi} \vec{x}_2 - \frac{L}{R} A_3 \dot{\varphi}^2 \vec{y}_2 + B_3 \ddot{\varphi} \vec{e}_2$$

$$4] \{T_{1 \rightarrow 2}\} = \begin{Bmatrix} x_A & L_A \\ y_A & \sigma_A \\ 0 & 0 \end{Bmatrix}_{A, B_2} \quad \{T_{2 \rightarrow 3}\} = \begin{Bmatrix} x_C & 0 \\ y_C & \sigma_C \\ z_C & N_C \end{Bmatrix}_{C, B_2}$$

$$\{T_{1 \rightarrow 3}\} = \begin{Bmatrix} 0 & 0 \\ y_n & 0 \\ z_n & 0 \end{Bmatrix}_{n, B_2}$$

$$5] \text{ Sur axe } (2+3), \text{ TRD sur } \vec{f}_1 : \begin{cases} z_n - (m_2 + m_3)g = 0 \\ z_n = (m_2 + m_3)g \end{cases}$$

$$6] \text{ Sur axe } (3), \text{ TRD sur } (G_1, \vec{x}_2) : \begin{cases} -\frac{L}{R} A_3 \ddot{\varphi} = y_n \cdot R \\ \Rightarrow y_n = -\frac{L}{R^2} A_3 \ddot{\varphi} \end{cases}$$

7] Adhérence n. |  $T < fN$

$$|y_n| < f |z_n| \Rightarrow \frac{|y_n|}{|z_n|} < f \Rightarrow \frac{\frac{L A_3 \ddot{\varphi}}{R^2 (m_2 + m_3) g}}{1} < f$$

(2)

Acceleration max  $\Rightarrow \ddot{\varphi} < \frac{R^2(m_2+m_3)g}{L A_3}$

$$\begin{aligned} 8] \vec{S}(A, 3/1) &= \vec{S}(a, 3/1) + \vec{AG} \wedge \vec{R}_L(3/1) \\ &= \dots + L \vec{x}_2 \wedge m_2 L (\ddot{\varphi} \vec{y}_2 - \dot{\varphi}^2 \vec{x}_2) \\ &= \dots + m_3 L^2 \ddot{\varphi} \vec{z}_2 \\ &= -\frac{L}{R} A_3 \ddot{\varphi} \vec{x}_2 - \frac{L}{R} A_3 \dot{\varphi}^2 \vec{y}_2 + (B_3 + m_3 L^2) \ddot{\varphi} \vec{z}_2 \end{aligned}$$

9] On isole (2+3), TAD sur (A, 3/1)

$$(C_2 + B_3 + m_3 L^2) \ddot{\varphi} = C_m + L \cdot Y_{11}$$

avec  $Y_{11} = -\frac{L}{R^2} A_3 \ddot{\varphi}$

$$\Rightarrow C_m = \left( C_2 + B_3 + m_3 L^2 + A_3 \frac{L^2}{R^2} \right) \cdot \ddot{\varphi}$$

$$C_m = J_{eq} \cdot \ddot{\varphi} \quad J_{eq} : \text{Inertie equivalente.}$$

Rem : Si on rajoute des frottements visqueux sur la pivot entre 1 et 2  $\Rightarrow C_f = -\lambda \cdot \dot{\varphi}$

$$\Rightarrow C_m = J_{eq} \ddot{\varphi} + \lambda \cdot \dot{\varphi}$$

$$C_m = J_{eq} \dot{\omega} + \lambda \omega$$

Si on passe dans Laplace :  $C_m(\tau) = (J_{eq} \tau + \lambda) \Omega(\tau)$

$$\frac{\Omega(\tau)}{C_m(\tau)} = \frac{1}{J_{eq} \tau + \lambda} = H(\tau) \quad \text{premier ordre}$$

