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Correction DS PSI, TP, octobre 22

Stabilité, Contrôle PSI 22

Q1) Direction d'axe-verticale : $\left. \begin{array}{l} M_{d \max} = 3,5 \text{ mm} \\ M_{d \min} = -2,3 \text{ mm} \end{array} \right\} \begin{array}{l} \text{pl. on} \\ \text{vent} \\ + 0,2 \text{ mm} \end{array}$

Pla frontal $\left\{ \begin{array}{l} M_{y \max} = 0,2 \text{ mm} \\ M_{y \min} = -0,3 \text{ mm} \end{array} \right.$

Q2) $\vec{P}_0 P = \vec{P}_0 O_0 + \vec{O}_0 P = -L \vec{f}_0 + L \vec{f}_1 =$

$\vec{f}_1 = \cos \theta_y \vec{f}_0 + \sin \theta_y \vec{x}_1'$

$\vec{f}_1' = -\sin \theta_x \vec{y}_0 + \cos \theta_x \vec{f}_0 ; \vec{x}_1' = \vec{x}_0$

$\vec{f}_1 = \sin \theta_y \vec{x}_0 - \cos \theta_y \sin \theta_x \vec{y}_0 + \cos \theta_y \cos \theta_x \vec{f}_0 \quad (\times L)$

$\vec{P}_0 P = L \left[\sin \theta_y \vec{x}_0 - \cos \theta_y \sin \theta_x \vec{y}_0 + (\cos \theta_y \cos \theta_x - 1) \vec{f}_0 \right]$

$M_x = -L \cos \theta_y \sin \theta_x$

$M_y = L \sqrt{(\sin \theta_y)^2 + (\cos \theta_y \cos \theta_x - 1)^2}$

Q3) $M_x \approx -L \theta_x ; M_y \approx L \theta_y$

$\Delta \theta_x = \frac{M_{x \min} - M_{x \max}}{L} = \frac{-2,3 - 3,5}{0,3 \cdot 10^{-3}} = -0,019 \text{ rad}$

$\Delta \theta_y = \frac{M_{y \max} - M_{y \min}}{L} = \frac{0,2 + 0,3}{0,3 \cdot 10^{-3}} = 0,0017 \text{ rad.}$

$\Delta \theta_x \gg \Delta \theta_y \quad 0$

on peut négliger la rotation autour de $(0, \vec{y}_0)$

\Rightarrow on peut considérer la liaison s'ouvre ≈ 0

comme une joint d'axe $(0, \vec{x}_0)$

Q4) Compensation sur $(0, \vec{x}_0)$.

$$\textcircled{2} \quad \textcircled{Q5} \quad \vec{T}(C_3, 3/0) = \begin{bmatrix} A & & \\ & B & \\ & & A \end{bmatrix} \begin{bmatrix} 0 \\ \dot{\theta}_3 \\ \dot{\theta}_2 \end{bmatrix} = B \dot{\theta}_3 \vec{y}_2 + A \dot{\theta}_2 \vec{y}_2$$

$$\textcircled{Q6} \quad \vec{S}(C_3, 3/0) = -B \dot{\theta}_3 \dot{\theta}_2 \vec{x}_2 + B \ddot{\theta}_3 \vec{y}_2 + A \ddot{\theta}_2 \vec{y}_2$$

Q7) On isole (1, 2 + 3), TND en C_3 , dans B_1 Δ

$$\left\{ \begin{array}{l} \vec{x}_2 = \cos \theta_2 \vec{x}_1 + \sin \theta_2 \vec{y}_1 \\ \vec{y}_2 = -\sin \theta_2 \vec{x}_1 + \cos \theta_2 \vec{y}_1 \end{array} \right.$$

$$\left\{ \begin{array}{l} L_{01} = -B \dot{\theta}_3 \dot{\theta}_2 \cos \theta_2 - B \ddot{\theta}_3 \sin \theta_2 \\ P_{01} = -B \dot{\theta}_3 \dot{\theta}_2 \sin \theta_2 + B \ddot{\theta}_3 \cos \theta_2 \\ N_{01} = A \ddot{\theta}_2 \end{array} \right.$$

$$\textcircled{Q8} \quad \omega_3 = \text{cte} \Rightarrow \ddot{\theta}_3 = 0$$

$$\begin{aligned} \vec{\Pi}(C_3) &= \vec{\Pi}(P) + C_3 P \perp \ell_C \vec{y}_1 = \\ &= \vec{0} + (L \vec{y}_1 - L \cos \theta_2 \vec{y}_1 + L \sin \theta_2 \vec{y}_1) \perp \ell_C \vec{y}_1 \\ &= (L \cos \theta_2 - L) \ell_C \vec{x}_1 \end{aligned}$$

$$L_{01} + (L \cos \theta_2 - L) \ell_C = -B \omega_3 \dot{\theta}_2 \cos \theta_2$$

$$L_{01} = 0 \Rightarrow \dot{\theta}_2 = \frac{L - L \cos \theta_2}{B \omega_3 \cos \theta_2}$$

Q9) Pour que $\dot{\theta}_2$, P_{01} et N_{01} soient finies ...

$$\left\{ \begin{array}{l} \text{Pour } N_{01} \text{ finie} \Rightarrow \dot{\theta}_2 \text{ finie.} \\ \text{Pour } P_{01} \text{ finie} \Rightarrow \theta_2 \text{ finie.} \end{array} \right.$$

③ Q10 $t_{5\%} \approx 0,01 \text{ s} < 0,033 \text{ s}$; $\varepsilon(\infty) = 0$

Très rapide et précis, on peut donc dire $H_2(\omega) = 1 = K_2$

Q11 $\theta_2 = \frac{1}{\tau} K_2 (U - C \theta_2) \Rightarrow \tau \theta_2 = K_2 U - K_2 C \theta_2$

$$H_{\theta_2} = \frac{\theta_2}{U} = \frac{K_2}{\tau + K_2 C}$$

~~Avec $C(\tau) = K_{10}$~~ Entrée: $U(\tau) = \frac{1}{\tau}$ $\theta_2(\tau) = \frac{K_2}{\tau(\tau + K_2 C)}$

$$\lim_{t \rightarrow \infty} \theta_2(t) = \lim_{\tau \rightarrow 0} \tau \theta_2(\tau) = \lim_{\tau \rightarrow 0} \frac{K_2}{\tau + K_2 C}$$

Avec $C(\tau) = K_{10}$, $\lim_{t \rightarrow \infty} \theta_2(t) = \frac{1}{K_{10}}$

Avec $C(\tau) = K_{10} + \frac{K_{11}}{\tau}$; $\lim_{t \rightarrow \infty} \theta_2(t) = 0$

Q12 $\Omega_2 = K_2 \left(U - \frac{C}{\tau} \Omega_2 \right) \Rightarrow \tau \Omega_2 = K_2 U \tau - K_2 C \Omega_2$

$$H_{\Omega_2} = \frac{\Omega_2}{U} = \frac{K_2 \tau}{\tau + K_2 C} = \frac{K_2 \tau}{\tau + K_2 K_{10} + \frac{K_2 K_{11}}{\tau}}$$

$$H_{\Omega_2} = \frac{K_2 \tau^2}{\tau^2 + K_2 K_{10} \tau + K_2 K_{11}} = \frac{\frac{\tau^2}{K_{11}}}{\frac{\tau^2}{K_2 K_{11}} + \frac{K_{10}}{K_{11}} \tau + 1}$$

$$\omega_m = \sqrt{K_2 K_{11}} \Rightarrow K_{11} = \frac{\omega_m^2}{K_2} = 6 \text{ rad/s}$$

$$\frac{2\zeta}{\omega_m} = \frac{K_{10}}{K_{11}} \Rightarrow \frac{2\zeta}{\sqrt{K_2 K_{11}}} = \frac{K_{10}}{K_{11}}$$

$$\Rightarrow K_{10} = \frac{2\zeta \sqrt{K_{11}}}{\sqrt{K_2}} = 1,81 \text{ rad/s}$$

⑤

Q14) On isole (1 + 2 + 3), TAD sur (O_0, \vec{f}_0)

Effort ext : | Poids de m_1 et m_3
| Efforts rognés en O_0

$$\text{Q15) } \vec{f}(G_1, \gamma_0) = \begin{bmatrix} A_1 \\ A_1 \\ C_1 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ 0 \\ 0 \end{bmatrix} = A_1 \dot{\theta}_1 \vec{x}_1$$

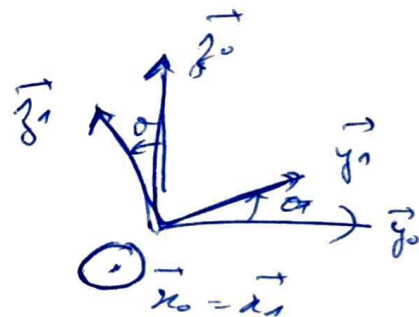
$$\vec{f}(G_1, \gamma_0) = A_1 \ddot{\theta}_1 \vec{x}_1$$

$$\vec{f}(O_0, \gamma_0) = \vec{f}(G_1, \gamma_0) + \underbrace{O_0 G_1}_{L_{G1}} \wedge m_1 \vec{a}(G_1 \in \gamma_0)$$

$$O_0 G_1 = L_{G1} \vec{y}_1$$

$$\vec{v}(G_1 \in \gamma_0) = -L_{G1} \dot{\theta}_1 \vec{y}_1$$

$$\vec{a}(G_1 \in \gamma_0) = L_{G1} (-\ddot{\theta}_1 \vec{y}_1 - \dot{\theta}_1^2 \vec{f}_1)$$



$$\vec{f}(O_0, \gamma_0) = (A_1 \vec{f}_1 + m_1 L_{G1}^2) \ddot{\theta}_1$$

$$\text{Q16) } O_0 G_3 = L_{G3} \vec{f}_1 + H_{G3} \vec{y}_1$$

$$\vec{v}(G_3 \in \gamma_0) = -L_{G3} \dot{\theta}_1 \vec{y}_1 + H_{G3} \dot{\theta}_1 \vec{f}_1$$

$$\vec{a}(G_3 \in \gamma_0) = (-L_{G3} \ddot{\theta}_1 \vec{y}_1 - H_{G3} \dot{\theta}_1^2) \vec{y}_1 + (H_{G3} \ddot{\theta}_1 - L_{G3} \dot{\theta}_1^2) \vec{f}_1$$

$$\text{Q17) } \vec{f}(G_3, \gamma_0) \cdot \vec{x}_0 = A_3 \ddot{\theta}_1 - B_3 \omega_3 \dot{\theta}_2$$

$$\vec{f}(O_0, \gamma_0) \cdot \vec{x}_0 = \vec{f}(G_3, \gamma_0) \cdot \vec{x}_0 + O_0 G_3 \wedge m_3 \vec{a}(G_3 \in \gamma_0)$$