

①

MP, Connexion DS de SI, octobre 26

Q1

$$\Delta L_2 = \Delta[AB]$$

$$AB = 1 - 0,52 - 0,285 = 0,195$$

Taille de 150 à 150 cm.

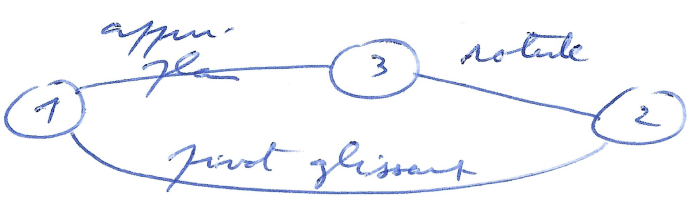
$$\Delta L_2 = 0,195 \times (150 - 150) = 7,8 \text{ cm}$$

$$\Delta L_3 = \Delta(BC)$$

$$BC = 0,285 - 0,035 = 0,256$$

$$\Delta L_3 = 0,256 \times (40) = 9,85 \text{ cm}$$

Q7

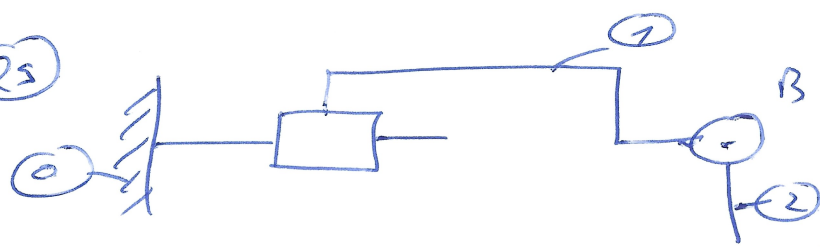


Q8

Clémère



Q9

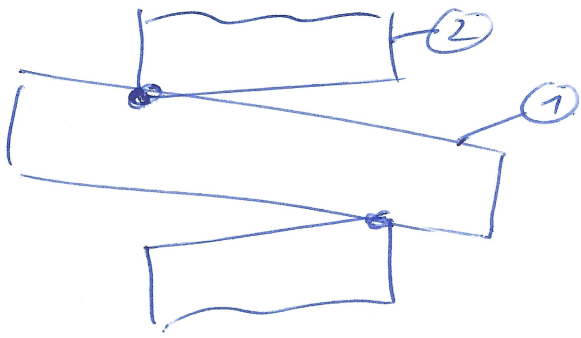


$$\{T_{1 \rightarrow 2}\} = \begin{Bmatrix} X & * \\ Y & * \\ 0 & 0 \end{Bmatrix}_B$$

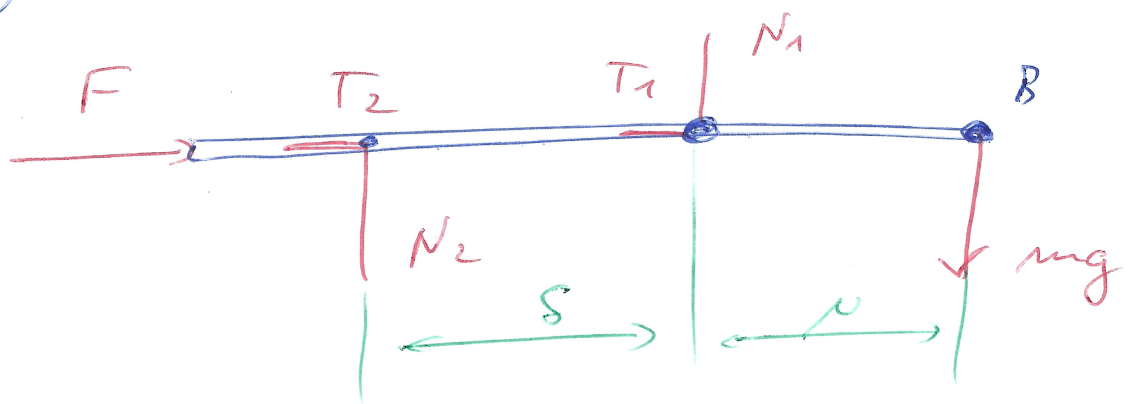
$$Y = mg$$

$$\{T_{\text{po} \rightarrow 2}\} = \begin{Bmatrix} 0 & * \\ -mg & * \\ + & 0 \end{Bmatrix}_B$$

Q10



Q11



②

PFS	$T_1 + T_2 = F$	<u>Limite glissement</u>	
	$N_1 = N_2 + mg$		$T_1 = \mu N_1$
	$N_2 \leq S = mg \times \mu$		$T_2 = \mu N_2$

5 equations, 5 inconnues : T_1, T_2, N_1, N_2, F

Calcul $\Rightarrow F = \mu mg \left(\frac{2\mu + 5}{5} \right)$

②12 Arc boutement.

②13 Calcul des charges $F < 150 \text{ N} \Rightarrow S < 89 \text{ mm}$

②14 $x = ; y = \dots$

②15 Basculement $\gamma_{02} < 0$

②25 $\vec{S}(G_2, \frac{1}{6}) = A_2 \vec{O}_1^2 \vec{S}$

3) Q25 $\vec{S}(A, \frac{2}{\%}) = A_2 \ddot{\theta}_1 \vec{z}$

$$\vec{A}G_2 = -\frac{L_2}{2} \vec{y}_1 ; \vec{v}(A, \frac{2}{\%}) = \frac{L_2}{2} \dot{\theta}_1 \vec{x}_1 ;$$

$$\vec{a}(A, \frac{2}{\%}) = \frac{L_2}{2} (\ddot{\theta}_1 \vec{x}_1 + \dot{\theta}_1^2 \vec{y}_1)$$

$$\begin{aligned} \vec{S}(A, \frac{2}{\%}) &= \vec{S}(G_2, \frac{2}{\%}) + \vec{A}G_2 \cdot m_2 \vec{a}(A, \frac{2}{\%}) \\ &= \left[A_2 + m_2 \left(\frac{L_2}{2} \right)^2 \right] \ddot{\theta}_1 \vec{z} \end{aligned}$$

de même : $\vec{S}(A, \frac{3}{\%}) = \left[A_3 + m_3 \left(L_2 + \frac{L_3}{2} \right)^2 \right] \ddot{\theta}_1 \vec{z}$

$$\vec{S}(A, \frac{4}{\%}) = \left[A_4 + m_4 (L_2 + L_3 + L_4)^2 \right] \ddot{\theta}_1 \vec{z}$$

$$\vec{S}(A, \frac{5}{\%}) = J_{\vec{z}} \ddot{\theta}_1 \quad \text{avec } J_{\vec{z}} = \dots$$

Q26 On isole (Σ_{+me}) TTD sur (A, \vec{z})

$$J_{\vec{z}} \ddot{\theta}_1 + J_m \dot{\omega}_m = C_1 - L_0 \rho_k g m_i \theta_1$$

Q27 On a $\omega_1 = k \omega_m$ et $C_1 = \frac{C_m}{k}$

$$J_{\vec{z}} k \dot{\omega}_m + J_m \dot{\omega}_m = \frac{C_m}{k} - L_0 \rho_k g m_i \theta_1$$

$$\underbrace{(J_{\vec{z}} k + J_m)}_{J_{\vec{z}}'} k \dot{\omega}_m = C_m - \underbrace{L_0 \rho_k g m_i \theta_1}_{a(t)}$$