

① Correction DS de SI, NP, de 25

Q2 Exigence 1.5 : réversibilité

Q3 1) Rotem ; 2) vis enrou 3) Colet came 4) Coilem 5) Position interne
6) P électrique 7) P mécanique (rotation) 8) P mécanique translation

Q4 $\vec{R}_2 = \vec{0}$

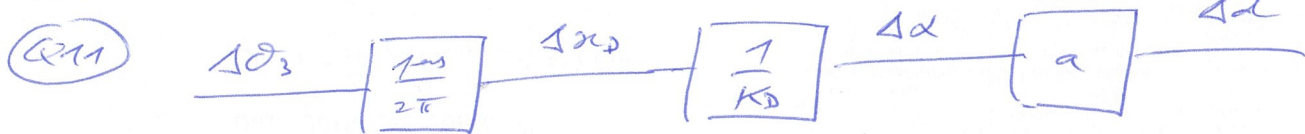
Q7 $d = 2(y_A + x_B \sin \alpha + y_B \cos \alpha)$

Q8 $\cos \alpha \approx 1 ; \sin \alpha \approx \alpha ; a = -150 \text{ mm} \cdot \text{rad}^{-1} ; b = 8,6 \text{ mm}$

Q9 Fermature géo en projection sur y_2^{\rightarrow} $\Rightarrow d_1 = x_E$

$d_2 = y_C - y_A ; d_3 = R_g ; d_4 = x_C$

Q10 Courbe $\Rightarrow K_D = 22,5 \text{ mm} \cdot \text{rad}^{-1}$



$\Delta \theta_3 = \frac{2\pi}{70^{14}} \text{ (coilem)}$ $\Delta d = \frac{a \times 70}{2\pi K_D} \Delta \theta_3 = 0,06 \mu\text{m}$

Q12 $R_{sg} \Rightarrow \vec{v}(I \in \Sigma_A) = \vec{0} = \underbrace{\vec{v}(I \in \Sigma_C)}_{\text{par C}} - \underbrace{\vec{v}(I \in \Sigma_A)}_{\text{par A}}$

On projette sur x_2^{\rightarrow}

$\Rightarrow \omega_{C_0} = \frac{\dot{\alpha} (K_D \cos(\alpha + \beta) - x_E \sin \alpha)}{R_g} = \frac{\dot{\alpha} (K_D - \sqrt{3} \cdot x_E)}{2 \cdot R_g}$

Q13 $E_c(\Sigma_0) = 2 \times \frac{1}{2} I_1 \dot{\alpha}^2 + \frac{1}{2} m_2 \dot{x}_D^2 + \frac{1}{2} I_3 \dot{\theta}_3^2 + 2 \times \left(\frac{1}{2} m_1 \dot{x}_D^2 + \frac{1}{2} I_4 \omega_{C_0}^2 \right)$

Q14 $\dot{\alpha} = \frac{70}{2\pi K_D} \dot{\theta}_3 ; \dot{x}_D = \frac{70}{2\pi} \dot{\theta}_3 ; \omega_{C_0} = K_D \dot{\alpha} = \dots$

$E_c(\Sigma_0) = \frac{1}{2} \left[2I_2 \left(\frac{70}{2\pi K_D} \right)^2 + (m_2 + 2m_1) \left(\frac{70}{2\pi} \right)^2 + I_3 + 2I_4 \left(\frac{K_D 70}{2\pi K_D} \right)^2 \right] \dot{\theta}_3^2$

Q15 Pentes : $P_{\text{rot}} = C_m \cdot \dot{\theta}_3^2 ; P_{\text{tr}} = -q \cdot \dot{\theta}_3^2$

$P_{\text{prop}} = -2a \alpha \dot{\alpha}$

(2) $P_{\text{objet 1}} = P(\text{objet} \rightarrow \%) = \vec{F}_{\text{objet 1}} \cdot \vec{v}(B \in \%)$

$\vec{F}_{\text{objet}} = F_0 \vec{y}_0$

$\vec{AB} = x_B \vec{x}_1 + y_B \vec{y}_1$

$\vec{v}(B \in \%) = x_B \dot{\alpha} \vec{y}_1 - y_B \dot{\alpha} \vec{x}_1$

$P_{\text{objet 1}} = F_0 \dot{\alpha} (x_B \cos \alpha - y_B \sin \alpha) \approx F_0 \dot{\alpha} x_B$

$P_{\text{objet 1}'} = -F_0 \dot{\alpha}' x_B = F_0 \dot{\alpha} x_B$

$P_{\text{objet}} = 2 F_0 \dot{\alpha} x_B$

de même $P_{\text{main}} = -2 F_m \dot{\alpha} x_E$

(Q16) $P_{\text{int}} = 0$

(Q17) $J_{\text{eq}} \ddot{\theta}_3 = C_m \dot{\theta}_3 - \underbrace{q \dot{\theta}_3^2 - 2 C_a \dot{\alpha} + 2 F_0 \dot{\alpha} x_B - 2 F_m \dot{\alpha} x_E}_{\dot{\alpha}}$

$\dot{\alpha} = \frac{1 \text{ rad}}{2\pi \text{ Kd}} \dot{\theta}_3$ $- 2 C_a \left(\frac{1 \text{ rad}}{2\pi \text{ Kd}}\right)^2 \theta_3 \dot{\theta}_3 + 2 F_0 x_B \left(\frac{1 \text{ rad}}{2\pi \text{ Kd}}\right)$
 $+ 2 (F_0 x_B - F_m x_E) \left(\frac{1 \text{ rad}}{2\pi \text{ Kd}}\right) \dot{\theta}_3$

$\Rightarrow J_{\text{eq}} \ddot{\theta}_3 + q \dot{\theta}_3 + 2 C_a \left(\frac{1 \text{ rad}}{2\pi \text{ Kd}}\right)^2 \theta_3 = C_m + 2 (F_0 x_B - F_m x_E) \frac{1 \text{ rad}}{2\pi \text{ Kd}} \dot{\theta}_3$

~~(Q18)~~ $J_{\text{eq}} \ddot{\theta}_3 + f_{\text{eq}} \dot{\theta}_3 + C_{\text{eq}} \theta_3 = -l_m F_m + l_0 F_0 + C_m$

(Q18) Pince bloquée sans objet : $\theta_3 = \text{cte}$ et $F_0 = 0$

$\Rightarrow C_m = C_{\text{eq}} \theta_3 + l_m F_m$

(Q19) Pince bloquée sans action millimètre : $\theta_3 = \text{cte}$ et $F_m = 0$

$\Rightarrow C_m = C_{\text{eq}} \theta_3 - l_0 F_0$

(Q20)

$$\textcircled{Q9} \quad \vec{OA} + \vec{AE} + \vec{EI} = \vec{OC} + \vec{CI}$$

$$y_A \vec{y}_0 + x_E \vec{x}_1 + x_I \vec{x}_2 = x_D \vec{x}_0 + x_C \vec{x}_0 + y_C \vec{y}_0 + R_g \vec{y}_2$$

x_1 et x_D variables, il faut éliminer x_1

ou projette sur \vec{y}_2

$$y_A \cos(\alpha + \beta) - x_E \sin \beta = -x_D \sin(\alpha + \beta) - x_C \sin(\alpha + \beta) + y_C \cos(\alpha + \beta) + R_g$$

$$x_D = \frac{x_E \sin \beta + (y_C - y_A) \cos(\alpha + \beta) + R_g}{\sin(\alpha + \beta)} - x_C$$

$$\textcircled{Q10} \quad x_D = K_D \cdot \alpha \Rightarrow K_D = \frac{\Delta x_D}{\Delta \alpha} = \frac{1}{0,045} = 22,2 \text{ mm/rad}$$



$$\alpha = \frac{1}{K_D} x_D = \frac{1 \text{ pas}}{2\pi K_D} \theta_3$$

Calcul : $2\pi \rightarrow 10$ position
 $\Delta \theta_3 = \frac{2\pi}{10^{14}} \rightarrow 1$ position

$$\Delta \alpha = \frac{1 \text{ pas}}{2\pi K_D} \frac{2\pi}{10^{14}} = \frac{1 \text{ pas}}{K_D \cdot 10^{14}}$$

$$\Delta \alpha = \frac{1 \text{ pas}}{22,2 \times 10^{14}}$$

$$\Delta d = a \Delta \alpha = \frac{a \times 1 \text{ pas}}{K_D \cdot 10^{14}} = 0,66 \text{ nm}$$

$$\textcircled{Q12} \quad \vec{v}(\Gamma \in \mathcal{E}_1) = \vec{0} = \vec{v}(\Gamma \in \mathcal{E}_0) - \vec{v}(\Gamma \in \mathcal{E}_0)$$

$$\begin{aligned} \vec{v}(\Gamma \in \mathcal{E}_0) &= \vec{v}(A \in \mathcal{E}_0) + \vec{\Omega}_{\mathcal{E}_0} \wedge \vec{AI} \\ &= \dot{x}_D \vec{x}_0 + \omega_{k1} \vec{z}_0 \wedge R_y \vec{y}_2 \\ &= \dot{x}_D \vec{x}_0 - \omega_{k1} R_y \vec{x}_2 \end{aligned}$$

$$\begin{aligned} \vec{v}(\Gamma \in \mathcal{E}_0) &= \vec{v}(A \in \mathcal{E}_0) + \vec{\Omega}_{\mathcal{E}_0} \wedge \vec{AI} \\ &= \vec{0} + \dot{\alpha} \vec{z}_0 \wedge (x_E \vec{x}_1 + x_1 \vec{x}_2) \\ &= \dot{\alpha} (x_E \vec{y}_1 + x_1 \vec{y}_2) \end{aligned}$$

$$\Rightarrow \dot{x}_D \vec{x}_0 - \omega_{k1} R_y \vec{x}_2 = \dot{\alpha} (x_E \vec{y}_1 + x_1 \vec{y}_2)$$

Rem : $\omega_{k1} = \omega_{k0}$; x_1 variable ; on projette sur \vec{x}_2

$$\begin{aligned} \dot{x}_D \cos(\alpha + \beta) - \omega_{k0} R_y &= \dot{\alpha} x_E \sin \alpha && \text{K}_D \dot{\alpha} \\ \omega_{k0} &= \frac{-\dot{\alpha} x_E \sin \alpha + \dot{x}_D \cos(\alpha + \beta)}{R_y} && \text{''} \end{aligned}$$

$$\text{R}_1, \alpha \text{ petit} \Rightarrow \omega_{k0} = \dot{\alpha} \left(\frac{K_D \cos(\alpha + \beta) - x_E \sin \alpha}{R_y} \right)$$

$$\left. \begin{array}{l} \alpha \text{ petit} \\ \beta = \frac{\pi}{3} \end{array} \right\} \Rightarrow \omega_{k0} = \dot{\alpha} \frac{K_D - \sqrt{3} x_E}{2 R_y}$$