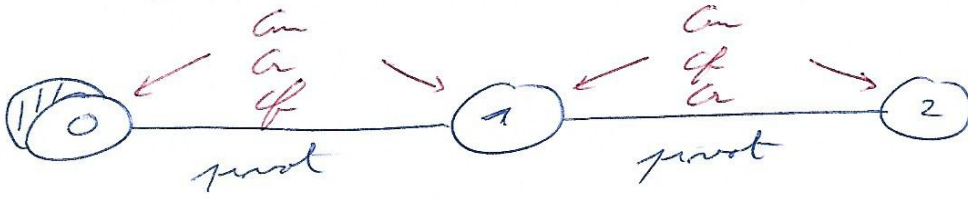


①

Mesures Topographique (contrôle NP17)

Q1



Q2 On isole (1+2), TPD sur (O, \vec{z}_1) .
 On isole (2), TPD sur (O, \vec{x}_1)) Ce qui correspond
 à une d° de liberté du mécanisme

Q3 On isole (1+2), TPD sur (O, \vec{z}_1) .

Moment cinétique : $\vec{T}(O \in \mathcal{Z}_0) = J_{z_1} \dot{\varphi} \cdot \vec{z}_0$

Moment dynamique : $\vec{\delta}(O \in \mathcal{Z}_0) = J_{z_1} \ddot{\varphi} \cdot \vec{z}_0$

Pour le solide (2) :

$\vec{T}(O \in \mathcal{Z}_0) = \vec{I}(O, 2) \cdot \vec{\Omega}_{\mathcal{Z}_0}^2$ (pas de terme complémentaire)

$\vec{\Omega}_{\mathcal{Z}_0}^2 = \dot{\varphi} \vec{z}_1 + \dot{\theta} \vec{x}_2 = \dot{\theta} \vec{x}_2 + \dot{\varphi} \sin \theta \vec{y}_2 + \dot{\varphi} \cos \theta \vec{z}_2$

$$\vec{T}(O \in \mathcal{Z}_0) = \begin{bmatrix} J_{x_2} & & \\ & J_{y_2} & \\ & & J_{z_2} \end{bmatrix} \begin{bmatrix} \dot{\theta} \\ \dot{\varphi} \sin \theta \\ \dot{\varphi} \cos \theta \end{bmatrix} = J_{x_2} \dot{\theta} \vec{x}_2 + J_{y_2} \dot{\varphi} \sin \theta \vec{y}_2 + J_{z_2} \dot{\varphi} \cos \theta \vec{z}_2$$

On cherche : $\vec{\delta}(O \in \mathcal{Z}_0) \cdot \vec{z}_1$, on utilise :

$$\vec{\delta}(O \in \mathcal{Z}_0) \cdot \vec{z}_1 = \left(\frac{d}{dt} \vec{T}(O \in \mathcal{Z}_0) \cdot \vec{z}_1 \right)_O - \vec{T}(O \in \mathcal{Z}_0) \cdot \left(\frac{d \vec{z}_1}{dt} \right)_O$$

$$\vec{T}(O \in \mathcal{Z}_0) \cdot \vec{z}_1 = J_{y_2} \dot{\varphi} \sin^2 \theta + J_{z_2} \dot{\varphi} \cos^2 \theta$$

On écrit le TPD \Rightarrow

$$\frac{R_1}{P_1} (C_{m1} + C_{r1} - C_{f1} \dot{\varphi}) = J_{z_1} \ddot{\varphi} + \frac{d}{dt} [(J_{y_2} \sin^2 \theta + J_{z_2} \cos^2 \theta) \dot{\varphi}]$$

② Enfinement : (1^{er} equation).

$$a_{m1} + a_{r1} = \frac{p_1}{b_1} J_{y1} \ddot{\varphi} + b_1 \dot{\varphi} + \frac{d}{dt} \left[\left(\frac{p_1}{b_1} J_{y2} m^2 \theta + \frac{p_1}{b_1} J_{y2} \cos^2 \theta \right) \dot{\varphi} \right]$$

On isole (2), TTD sur (O, x1)

Rappel : $\vec{V}(O \in \mathcal{R}_0) = J_{x2} \dot{\theta} \vec{x}_2 + J_{y2} \dot{\varphi} m \theta \vec{y}_2 + J_{y2} \dot{\varphi} \cos \theta \vec{z}_2$

On cherche $\vec{S}(O \in \mathcal{R}_0) \cdot \vec{x}_1$, on utilise :

$$\vec{S}(O \in \mathcal{R}_0) \cdot \vec{x}_1 = \left(\frac{d \vec{V}(O \in \mathcal{R}_0) \cdot \vec{x}_1}{dt} \right)_0 - \vec{V}(O \in \mathcal{R}_0) \cdot \left(\frac{d \vec{x}_1}{dt} \right)_0$$

$$\left(\frac{d \vec{x}_1}{dt} \right)_0 = \dot{\varphi} \vec{y}_1 \quad \text{et} \quad \vec{y}_1 = \cos \theta \vec{y}_2 - m \theta \vec{z}_2$$

$$\begin{aligned} \Rightarrow \vec{S}(O \in \mathcal{R}_0) \cdot \vec{x}_1 &= J_{x2} \ddot{\theta} + \dot{\varphi}^2 (J_{y2} m \theta \cos \theta - J_{y2} m \theta \cos \theta) \\ &= J_{x2} \ddot{\theta} + \dot{\varphi}^2 \frac{(J_{y2} - J_{z2})}{2} m (2\theta) \end{aligned}$$

Enfinement : 2^e equation.

$$\frac{b_2}{p_2} (a_{m2} + a_{r2} - p_2 \dot{\theta}) = J_{x2} \ddot{\theta} + \frac{J_{y2} - J_{z2}}{2} m (2\theta) \dot{\varphi}^2$$

$$a_{m2} + a_{r2} = \frac{p_2}{b_2} J_{x2} \ddot{\theta} + p_2 \dot{\theta} + \frac{p_2 (J_{y2} - J_{z2})}{b_2 \cdot 2} m (2\theta) \dot{\varphi}^2$$

$$\textcircled{Q5} \quad \underline{\theta=0} \Rightarrow \begin{cases} a_{m1} + a_{r1} = A_1 \ddot{\varphi} + B_1 \dot{\varphi} + C_1 \varphi \\ a_{m2} + a_{r2} = A_2 \ddot{\theta} + B_2 \dot{\theta} \end{cases}$$

$$\Rightarrow J_{y\varphi} = A_1 + C_1 \quad \text{et} \quad J_{y\theta} = A_2$$

On pense ramener les inerties au niveau des arbres moten

$$\Rightarrow E_1 = \frac{1}{2} J_{y\varphi} \dot{\varphi}^2 = \frac{1}{2} J_{y\varphi} \omega_{m1}^2 \Rightarrow J_{\varphi} = J_{y\varphi} \cdot A_1^2$$

$$\text{Idem pour } J_{\theta} = J_{y\theta} \cdot p_2^2$$